



DC and microwave characteristics of AlN spacer based $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}/\text{GaN}$ HEMT on SiC substrates for high power RF applications

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Abstract

The DC and RF performance of 30nm gate length enhancement mode (E-mode) AlGa_{0.37}N/GaN High electron mobility transistor (HEMT) on SiC substrate with heavily doped source and drain region have investigated using Synopsys TCAD tool drift diffusion model at room temperature. The proposed device features are recessed T - gate structure, InGa_{0.37}N back barrier and Si₃N₄ passivated device surface. The HEMT exhibits a maximum drain current density of 2.1 [A/mm], transconductance g_m of 1680 [mS/mm], current gain cut-off frequency f_t of 220 GHz and power gain cut-off frequency f_{max} of 245 GHz. At room temperature the measured carrier mobility (μ), sheet charge carrier density (n_s) and breakdown voltage are 1400 ($\text{cm}^2/\text{V} - \text{s}$), 1.6×10^{13} (Cm^{-2}) and 14 V respectively. The excellent DC and microwave performance of the proposed HEMT is promising candidate for future high power RF applications.

Keywords: HEMT, back-barrier, recessed gate, cut-off frequency, regrown ohmic contact and short channel effects.

1. Introduction

The preeminent physical property of GaN such as larger band gap (3.44 eV), breakdown field ($3.3 \times 10^6 \text{V/cm}$), higher saturation velocity ($2.7 \times 10^7 \text{cm/s}$), good thermal conductivity ($1.95 \text{Wcm}^{-1}\text{c}^{-1}$) and higher mobility ($\mu_n = 2000$ and $\mu_h = 200 \text{cm}^2/\text{V} - \text{s}$) [1-2] has captivated the raptness attentions to develop high power with high frequency very large scale integration (VLSI) circuits for next generation RF applications such as high power amplifiers for space research, remote sensing, imaging systems and low noise wide bandwidth amplifiers design. In the last two decade's several research progresses have been made to improve the DC and Microwave characteristics of GaN based HEMT [3-22]. The current gain cut-off frequency (f_t), power gain cut-off frequency (f_{max}) and breakdown voltage (V_{Br}) of the HEMT are important parameters for

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RF and mixed signal applications. Several progress has been made to improve the cut-off frequency of the GaN based HEMT such as InAlN/AlGaIn/AlN as top barrier, InGaIn/AlGaIn back barrier, regrown ohmic contacts and device surface passivation [3-14]. However the breakdown voltage of the device is deteriorated when the device is scaling down below 50 nm gate length. Breakdown voltage is an essential parameter for high power applications. The higher breakdown field of GaN is the motivation for designing GaN based power amplifiers monolithic microwave integrated circuits for Sub-millimeter wave applications. Smaller breakdown voltages limit the high power RF operation of the device. In addition to that higher f_{max} is required for high power amplifiers design. To enhance the f_{max} of the HEMT, proper device design is necessary in order to minimize the gate resistance (R_g), drain conductance (g_d) and gate-drain capacitance (C_{gd}), which will reduce the parasitic time delay of the device so that f_T and f_{max} of GaN based HEMT are improved significantly.

To improve the high frequency operation of the device the gate length (L_g) must be reduced for lower transit time of electrons. For the gate length below 50 nm device needs a thinner barrier layer to maintain the good aspect ratio L_g/d (gate length - gate to channel separation distance). Higher the aspect ratio results in suppressed drain induced barrier lowering (DIBL) [13].

A 80 nm gate length AlGaIn/GaN HEMT on Si manifested a maximum f_t/f_{max} of 176/70 GHz [1]. The SiN passivated 100 nm gate length conventional rectangular gate AlGaIn/GaN HEMT demonstrated a f_{max} 118 GHz [2] and also the minimum noise figure is demonstrated in [11] by using SiN passivation. T gate AlGaIn/GaN HEMT with 0.14 μm gate length had shown a power gain cut-off frequency of 35 GHz [3]. 100nm gate length AlGaIn/GaN HEMT with InGaIn back barrier obtained f_t/f_{max} of 153/198 GHz [4]. The heavily doped source/drain region n+ GaN regrown ohmic contacts with 50 nm T gate InAlN/GaN HEMTs on SiC demonstrated f_t/f_{max} of 141/232 GHz [10]. High on/off current ratio is achieved by 50 nm gate length InAlN/GaN HEMT with SiN passivation [9]. With the improved transconductance and suppression of current collapses is demonstrated by using recessed gate AlGaIn/GaN and also the short channel effect is reduced in greater extent [13]. The improved breakdown voltage of the AlGaIn/GaN HEMT had shown by using AlGaIn back barrier [14]. The enhanced carrier confinement, higher mobility 1300 ($cm^2/V - s$), improved sheet resistance R_{sh} of 420 [Ω/Sqr] with reduced buffer leakage is demonstrated by using 3nm InGaIn back barrier in [20].

In this article, we have proposed and investigated the DC and RF characteristics of a novel 30 nm heavily doped (n+ GaN) regrown ohmic source/drain regions with recessed T-gate AlGaIn/AlN/GaN HEMT. To obtain the superior carrier confinement in 2DEG with enhanced carrier mobility, $In_{0.15}Ga_{0.85}N$ is used as back barrier in our model. The parasitic gate capacitances are majorly suppressed by SiN passivation layer. The higher aspect ratio is maintained (L_g/d) by recessed gate structure to effectively reduce the short channel effects. The proposed novel $L_g=30$ nm AlGaIn/GaN HEMT device shows an excellent improvement in DC and RF characteristics. The peak drain current density I_d of 2.1 [A/mm], g_m of 1680 [mS/mm], and f_t/f_{max} of 220/245 GHz are recorded. The observed off-state breakdown voltage of the device is 14V. The gate leakage current and SCEs are majorly suppressed and improved on/off ratio is achieved. These high DC and RF performances of the HEMT are obtained because of extreme reduction in the device parasitic resistances and capacitances.

2. Device structure and Bandgap diagram:

The vertical cross section of *AlGaN/AiN/GaN HEMT* device structure is depicted in Fig.1. The device consists of 3 inch SiC substrate to achieve good thermal stability, 1450 nm Fe doped GaN buffer layer, which isolates the channel from the substrate defects, 3.5 nm *InGaN* back barrier layer, which helps to confine more electron in the channel due to its effective conduction band notch at the interface with *GaN* channel and also it contributed for higher carrier mobility in the 2DEG ($\sim 1500 \text{ cm}^2/\text{V} - \text{S}$). Moreover the buffer leakage current is suppressed by the *InGaN* back barrier. The channel region is defined by 30 nm *GaN* and 10 nm $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}$ is used as the top barrier layer. A very thin 1 nm *AlN* spacer layer is placed between the barrier and channel which improves the electron mobility in the 2DEG by reducing the interface roughness and alloy disorder scattering at the interface of *AlGaN/GaN*. The source and drain regions are formed by heavily doped *GaN* (50 nm) with *Si* in the order of $\sim 7 \times 10^{20} \text{ cm}^{-3}$ to minimize the contact resistances. The source and drain ohmic contacts are designed by using *Ti/Pt/Au* metal stack and T shaped recessed gate is formed by *Pt/Au* metal stack. T-gate structure having the head size of 400 nm, stem height of 140 nm with 20 nm footprint is designed, which lift-off wide cross sectional gate area with smaller gate length, and schottky contact is formed by *Ni/Pt/Au* metal stack. The drain to source separation is kept at 140 nm. In order to reduce the parasitic capacitances of the device, finally the device surface is fully passivated by 25 nm Si_3N_4 layer, which greatly helped for achieving higher cut-off frequencies and to avoid the current collapses.

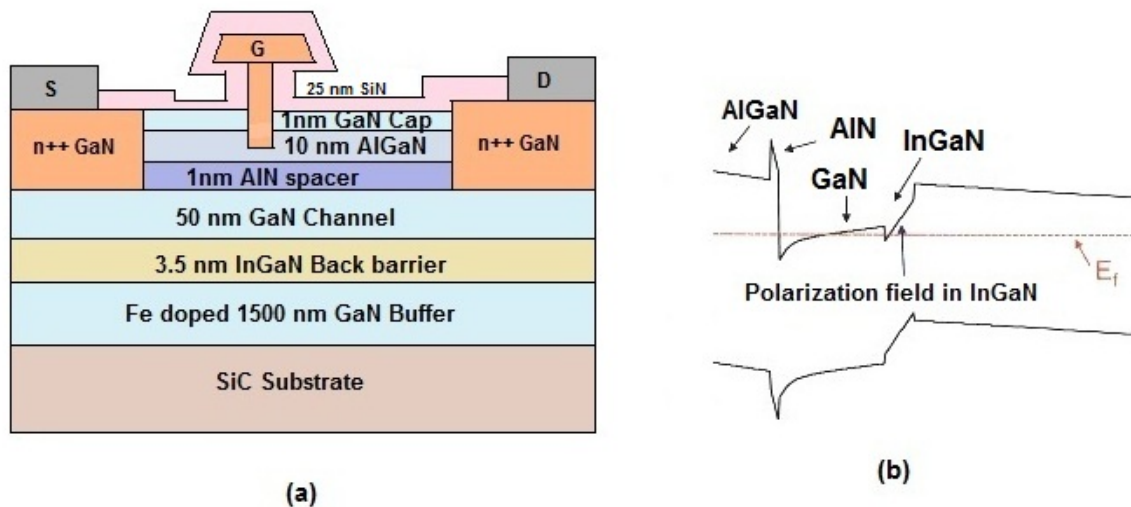


Fig.1: (a) AlGaN/AiN/GaN HEMT with InGaN back –barrier, (b) Conduction band offset.

The conduction band offset diagram of AlGaN/AiN/GaN/InGaN is depicted in Fig.1.b. Due to the induced piezoelectric polarization between InGaN and GaN, there will be a sharp raised potential barrier is formed at the back of 2DEG channel. Such a sharp notch helps to confine the electron in a better manner in the channel region and also it mitigates the buffer leakage current. A very thin 1 nm wide band gap (6.01 eV) AlN spacer is placed between barrier and channel to offer large effective conduction band offset and also it helps to reduce the gate leakage current.

3. Results and Discussion

Fig.2. shows the sheet charge carrier density, mobility and sheet resistance dependency on Al content in $Al_xGa_{(1-x)}N$ barrier layer [4]. Higher the Al content of barrier layer gives better sheet charge density but the mobility of the carriers is decreasing. In this work, a 10 nm $Al_{0.37}Ga_{0.63}N$ barrier layer with InGaN back barrier offered a sheet carrier density of $1.6 \times 10^{13} \text{ Cm}^{-2}$ and the observed mobility of electron in the 2DEG from the device structure simulation is $1450 \text{ cm}^2/\text{V} - \text{s}$. The back barrier layer greatly helped to confine the electron in 2DEG region in better manner and enhanced the sheet charge density.

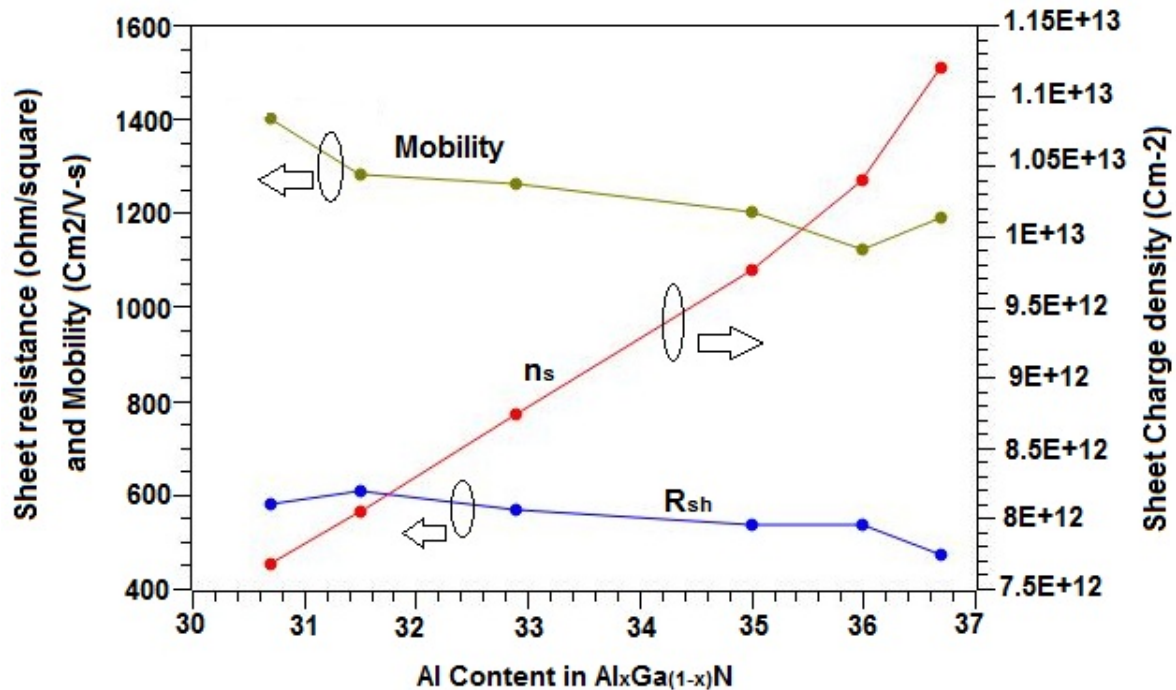


Fig.2: Sheet charge density, mobility, sheet resistance dependency on Al content in $Al_xGa_{(1-x)}N$ Barrier layer [2].

Fig.3. shows the $V-I$ characteristics of $L_g = 30 \text{ nm}$ and $w = 2 \times 27 \mu\text{m}$ E -mode $AlGaN/AlN/GaN$ HEMT. The simulation result gives a supreme drain current of 2.1 [A/mm] at $V_{gs} = 2\text{V}$ and the device is pinched off perfectly at $V_{gs} = 0\text{V}$. The extracted very low on resistance (R_{on}) of the device for $V_{gs} = 2\text{V}$ is $0.27 \text{ ohm} - \text{mm}$. This higher current density is achieved mainly because of the enhanced mobility with greater sheet charge carrier density in 2DEG channel. The $InGaN$ back barrier notch helps to provide the better confinement of charge carrier in channel and also it suppressed the buffer leakage current in the device. A 14 V off state breakdown voltage is obtained from the breakdown characteristics Fig.4.

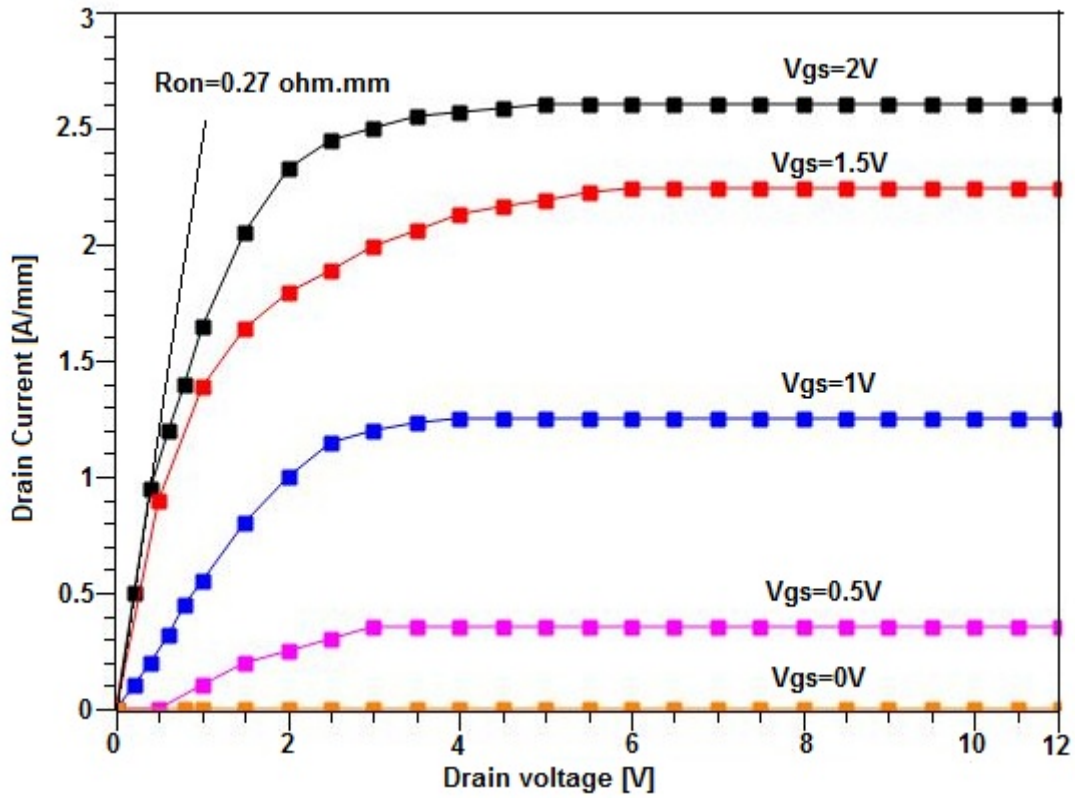


Fig.3: V-I Characteristics of $L_g = 30$ nm and $w = 2X27 \mu m$ E-mode AlGaIn/AIn/GaN HEMT

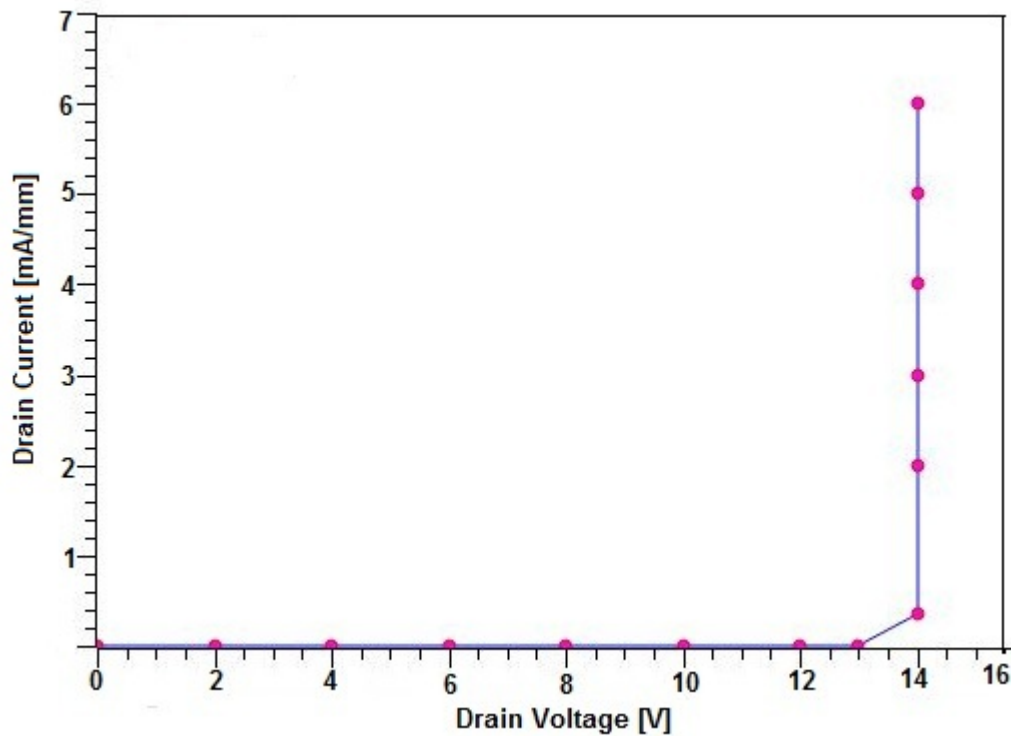


Fig. 4: off state-breakdown characteristics of $L_g = 30$ nm and $w = 2X27 \mu m$ E-mode AlGaIn/AIn/GaN HEMT .

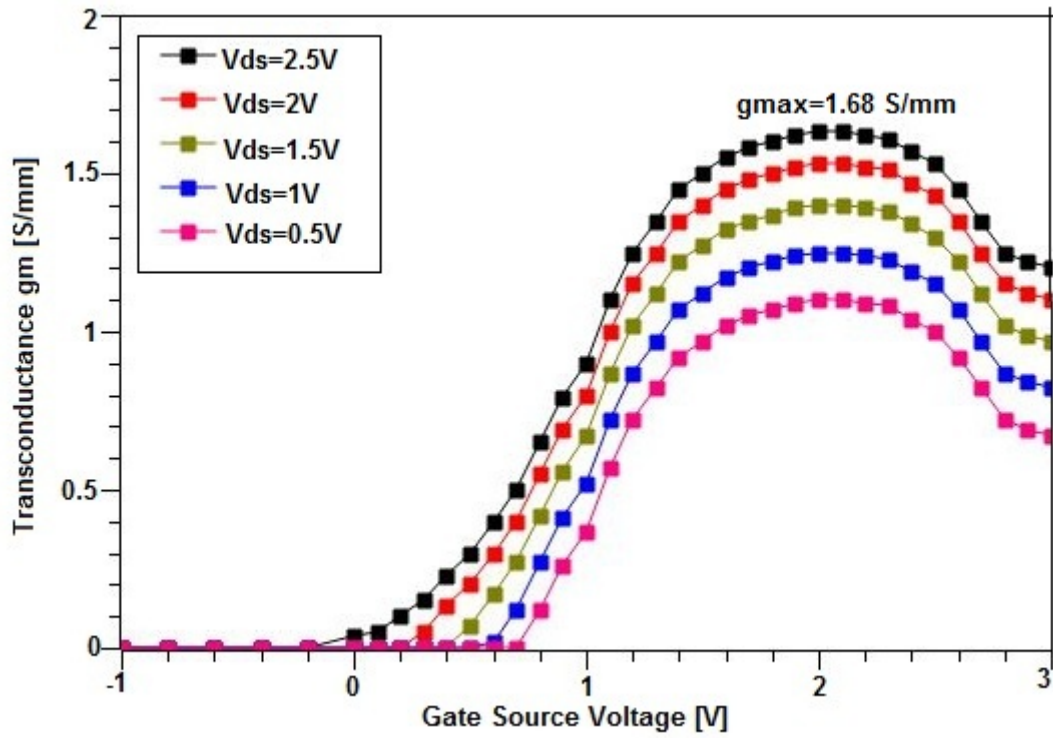


Fig.5: Dependences of g_m on the gate bias of $L_g = 30$ nm and $w = 2 \times 27 \mu m$ E-mode AlGaIn/AlN/GaN HEMT.

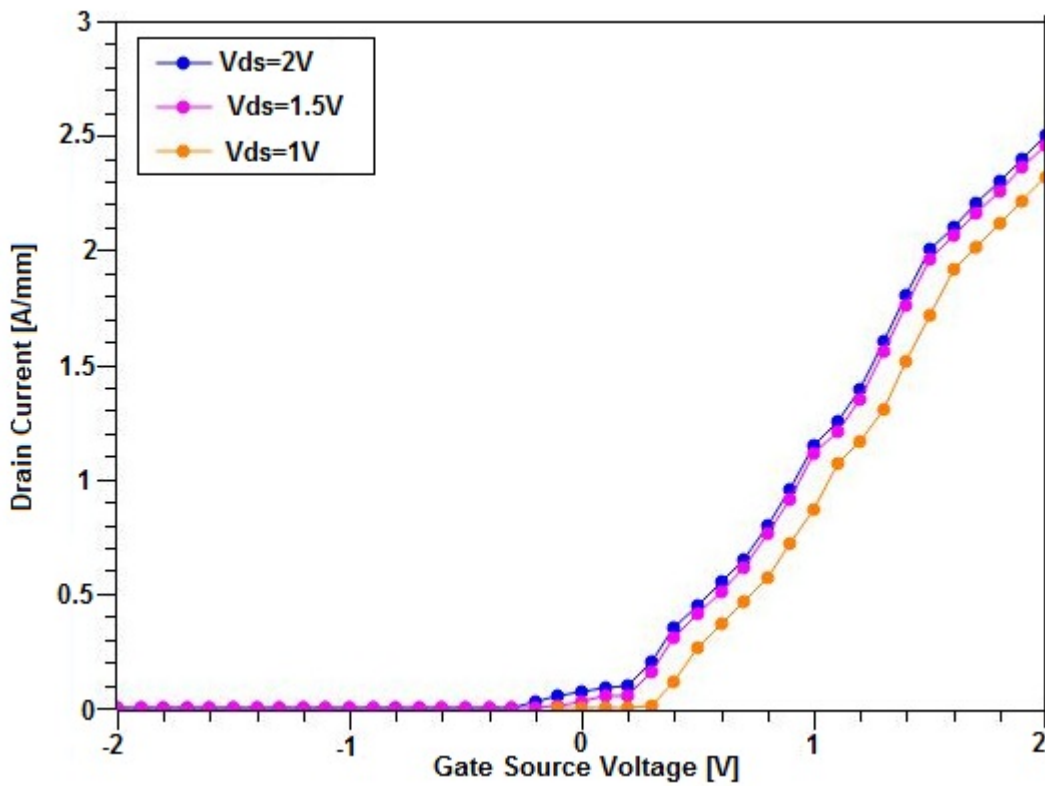


Fig.6: Dependences of I_d on the gate bias of $L_g = 30$ nm and $w = 2 \times 27 \mu m$ E-mode AlGaIn/AlN/GaN HEMT.

Fig.5. shows the transconductance variation with the gate bias voltage. The maximum transconductance of the device is extracted from the plot is 1.68 (S/mm) at $V_{gs} = 2V$. The extracted threshold voltage of the device from the transfer characteristics Fig.6. ($I_{ds} - V_{gs}$) is $-0.4V$.

The subthreshold and gate leakage current characteristics of $L_g = 30 \text{ nm}$ and $w = 2X27 \mu\text{m}$ E-mode AlGaIn/AlN/GaN HEMT is shown in Fig.7. The gate leakage current depends on the band gap of the barrier and channel materials. The higher the band gap AlN spacer layer effectively suppressed the gate leakage current in the order of $1X10^{-9} \text{ A/mm}$ at $V_{gs} = 0V$. The drain current on/off ratio is observed as 10^6 at $V_{ds} = 2V$.

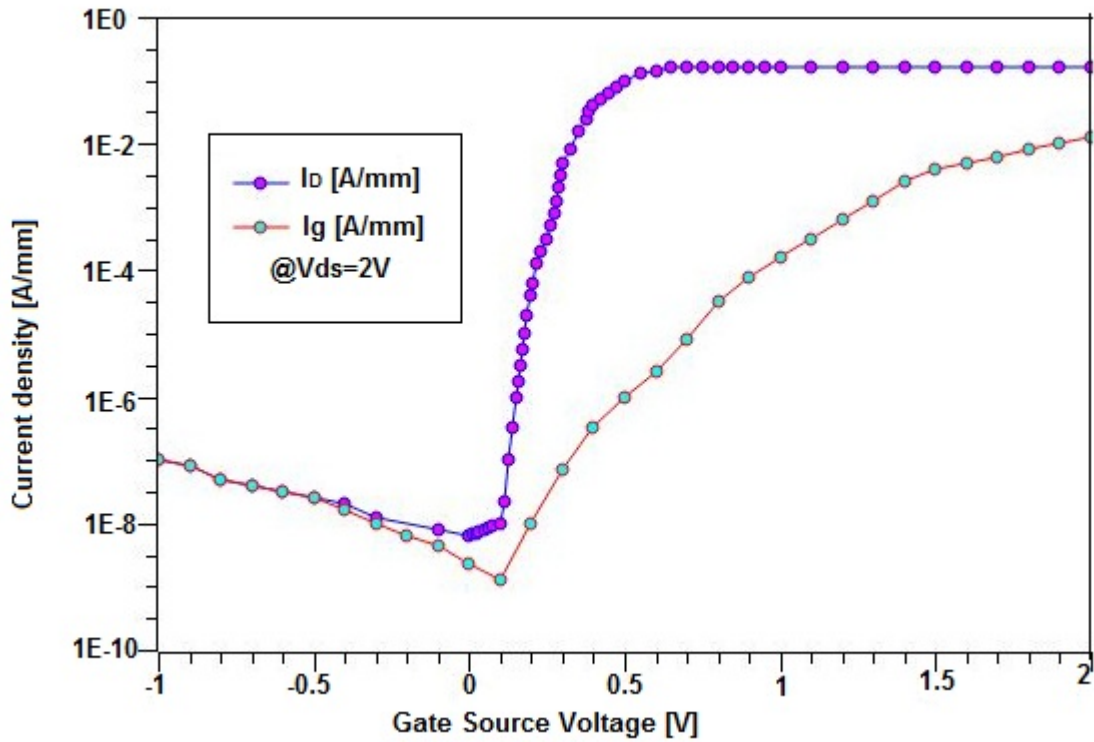


Fig. 7: Subthreshold and gate leakage current characteristics of $L_g = 30 \text{ nm}$ and $w = 2X27 \mu\text{m}$ E-mode AlGaIn/AlN/GaN HEMT in log-scale plot.

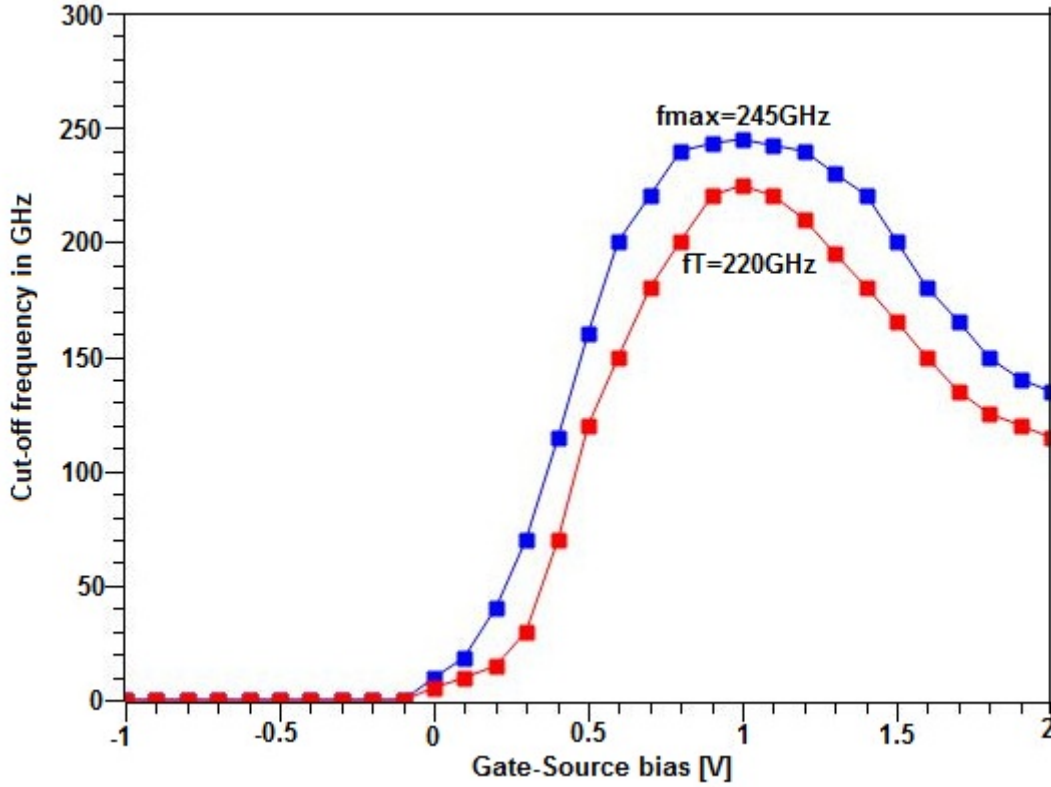


Fig.8: Cut-off frequencies Vs gate bias of $L_g = 30 \text{ nm}$ and $w = 2X27 \mu\text{m}$ E-mode AlGaIn/AlN/GaN HEMT for $V_{ds}=2\text{V}$.

The simulation result of current gain cut-off frequency (f_t) and power gain cut-off frequency (f_{max}) of $L_g = 30 \text{ nm}$ AlGaIn/AlN/GaN E – HEMT is displayed in Fig.8. The obtained peak f_t/f_{max} is 220/245GHz respectively. The obtained cut-off frequencies are the best cut-off frequencies of enhancement mode AlGaIn/GaN HEMTs with peak drain current of 2.1 [A/mm] , low gate leakage current and high on-off ratio among any AlGaIn/GaN device structure so far from author’s knowledge. The higher f_t/f_{max} is achieved by a drastic reduction in the contacts resistances and parasitic capacitance of the device mainly because of heavily doped ($n++\text{GaIn}$) source / drain regions has direct contacts with the channel, combined with $\sim 50\text{nm}$ drain and source access region and passivated device surface. The features of recessed T-gate structure is escalated transconductance (g_m) and the attenuated drain conductance also contributed to achieve this higher f_t and f_{max} . The expression for f_t and f_{max} are written as follows;

$$\text{Current gain Cut-off frequency } f_t = \frac{g_m/g_{ds}}{2\pi\left(\left((C_{gs}+C_{gd})+\left(\frac{1}{g_{ds}+(R_s+R_d)}\right)\right)+(C_{gd}\cdot g_m/g_{ds})(R_s+R_d)\right)} \quad (1)$$

$$\text{Power gain cut-off frequency } f_{max} = \frac{f_t}{2\sqrt{(R_s+R_g)g_{ds}+2\pi f_t R_g C_{gd}}} \quad (2)$$

where the source resistance $R_s = \left(\frac{R_c}{w}\right) + \left(\frac{R_{sh}\cdot L_{GS}}{w}\right)$ and drain resistance $R_d = \left(\frac{R_c}{w}\right) + \left(\frac{R_{sh}\cdot L_{SD}}{w}\right)$. R_c is the contact resistance and R_{sh} denotes the channel sheet resistance, respectively. L_{GS} is the gate to source distance and L_{SD} is the gate to drain separation, respectively. w is the width of the gate. R_g is the gate access resistance and g_{ds} represents

the drain conductance. The gate to drain capacitance C_{gd} is the essential parameter for high frequency operation of the device. A 25 nm SiN passivated device surface reduces the overall gate capacitance in our proposed device model. The extracted small signal parameters transconductance g_m , drain conductance g_{ds} , gate-source capacitance C_{gs} , gate-drain capacitance C_{gd} , source resistance R_s , drain resistance R_d , subthreshold slope (SS), Sheet resistance R_{sh} and on resistance R_{on} of the 30 nm recessed T gate AlGaIn/AlN/GaN HEMT device with heavily doped source and regions are 1.68 S/mm, 0.17 S/mm, 821 fF/mm, 178 fF/mm, 0.23 ohm-mm, 0.26 ohm-mm, 90 mV/dec, 490ohm/sqr and 0.27 ohm-mm, respectively. The comparison of our simulation result with various experimental results for different gate lengths is shown in Table.1. The 50 nm InAlN/GaN HEMT [7] had shown the f_{max} of 231 GHz but the breakdown voltage of the device is less than 10V. In this work, the higher cut-off frequencies is achieved with 14V off-state breakdown voltage for 30 nm gate length.

Table 1: I_d , g_m , f_{max} , f_t , gate leakage current and on/off ratio for various gate length InAlN/GaN HEMTs.

References	Gate length	f_{max} GHz	f_t GHz
[3], 2015	80 nm	70	176
[4],2013	100 nm	118	80
[5],2015	0.14 μm	35	63
[6],2006	100 nm	198	153
[7],2005	160 nm	170	130
[10],2015	50 nm	232	141
This work	30 nm	245	220

4. Conclusion

The DC and RF characteristics of a novel 30 nm recessed T-gate AlGaIn/AlN/GaN HEMT with InGaIn back barrier have been studied by using Synopsys TCAD . The simulation is performed by using physics based drift-diffusion model at room temperature. The device features are heavily doped ($n++$) source/drain regions with SiN passivated device surface, which helped us to reduce the contact resistances and gate capacitances of the device to uplift the microwave characteristics of the HEMTs. Lg of 30 nm HEMT shows a current gain cut-off frequency of 220 GHz and power gain cut-off frequency of 245 GHz. The peak drain current density of 2.1A/mm is achieved by offering effective conduction band offset by using AlN spacer associated with InGaIn back barrier to enhance the sheet charge carrier density in 2DEG region ($1.6 \times 10^{13} \text{ Cm}^{-2}$) with higher carrier mobility of 1400 ($\text{cm}^2/\text{V} - \text{s}$). The off-state breakdown voltage of the device is 14V. The recessed T-gate structure reduced the short channel effects ($SS = 90 \text{ mV/dec}$) by minimizing the gate to channel separation. The superior DC and RF performance of proposed HEMT device expected to be the most optimistic applicant for future high power sub-millimetre monolithic microwave integrated circuits applications.

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References

- [1] Liu William, Fundamentals of III–V devices HBT's, MESFETs, and HFETs/HEMTs. John Wiley & Sons, Inc.; 1999
- [2] Piprek Joachim. Nitride Semiconductor Devices Principles and Simulation. Weinheim: WILEY-VCH Verlag GmbH & Co KGaA; 2007
- [3] I.Wael Jatal, Uwe Baumann, Katja Tonisch, Frank Schwierz, and Jörg Pezoldt “High-Frequency Performance of GaN High-Electron Mobility Transistors on 3C-SiC/Si Substrates With Au-Free Ohmic Contacts” IEEE Electron device letters, **36** (2), February 2015. doi: 10.1109/LED.2014.2379664
- [4] Dirk Schwantuschke, Peter Brückner, Rüdiger Quay, Michael Mikulla and Oliver Ambacher “High-Gain Millimeter-Wave AlGaIn/GaN Transistors” IEEE Transactions on electron devices, vol. 60, no. 10, october 2013. doi: 10.1109/TED.2013.2272180
- [5] Robert C. et.al. “Implementation of High-Power-Density X-Band AlGaIn/GaN High Electron Mobility Transistors in a Millimeter-Wave Monolithic Microwave Integrated Circuit Process” IEEE electron device letters, **36** (10), october 2015. doi:10.1109/LED.2015.2474265
- [6] T. Palacios, A. Chakraborty, S. Heikman, S. Keller, S. P. DenBaars and U. K. Mishra, “AlGaIn/GaN High Electron Mobility Transistors With InGaIn Back-Barriers” IEEE Electron device letters, **27** (1), January 2006. doi: 10.1109/LED.2005.860882
- [7] T. Palacios, A. Chakraborty, S. Rajan, C. Poblenz, S. Keller, S. P. DenBaars, J. S. Speck and U. K. Mishra, “High-Power AlGaIn/GaN HEMTs for Ka-Band Applications” IEEE Electron device letters, **26** (11), November 2005. doi: 10.1109/LED.2005.857701
- [8] Faiza Afroz Faria, Jia Guo, Pei Zhao, Guowang Li, Prem Kumar Kandaswamy et al. “Ultra-low resistance ohmic contacts to GaN with high Si doping concentrations grown by molecular beam epitaxy” Appl. Phys. Lett. **101**, 032109 (2012); doi: 10.1063/1.4738768
- [9] Lorenzo Lugani, Jean-François Carlin, Marcel A. Py, Denis Martin, Francesca Rossi, Giancarlo Salviati, Patrick Herfurth, Erhard Kohn, Jürgen Bläsing, Alois Krost and Nicolas Grandjean “Ultrathin InAlN/GaN heterostructures on sapphire for high on/off current ratio high electron mobility transistors” Journal of Applied Physics **113**, 214503 (2013); doi: 10.1063/1.4808260
- [10] Diego Marti, Stefano Tirelli, Valeria Teppati, Lorenzo Lugani, Jean-François Carlin, Marco Malinverni, Nicolas Grandjean and C. R. Bolognesi “94-GHz Large-Signal Operation of AlInN/GaN High-Electron-Mobility Transistors on Silicon with Regrown Ohmic Contacts” IEEE Electron device letters, **36** (1), January 2015. doi: 10.1109/LED.2014.2367093
- [11] Z. H. Liu, S. Arulkumaran and G. I. Ng, “Improved Microwave Noise Performance by SiN Passivation in AlGaIn/GaN HEMTs on Si” IEEE Microwave and wireless components letters, **19** (6), June 2009. doi: 10.1109/LMWC.2009.2020027
- [12] Jia Guo et.al “MBE-Regrown Ohmics in InAlN HEMTs with a Regrowth Interface Resistance of $0.05 \Omega \cdot \text{mm}$ ” IEEE Electron device letters, **33** (4), April 2012. doi: 10.1109/LED.2012.2186116

- [13] Subramaniam ARULKUMARAN_, Takashi EGAWAY, Lawrence SELVARAJ and Hiroyasu ISHIKAWA “On the Effects of Gate-Recess Etching in Current-Collapse of Different Cap Layers Grown AlGa_N/Ga_N High-Electron-Mobility Transistors” Japanese Journal of Applied Physics , **45** (8), 2006, L220–L223.
- [14] Sheng Lei Zhao, Bin Hou, Wei Wei Chen, Min Han Mi, Jia Xin Zheng, Jin Cheng Zhang, Xiao Hua Ma and Yue Hao “Analysis of the Breakdown Characterization Method in Ga_N-Based HEMTs” IEEE Transactions on power electronics, **31** (2), February 2016. doi: 10.1109/TPEL.2015.2416773
- [15] Johan Bergsten, Jr-Tai Chen, Sebastian Gustafsson, Anna Malmros, Urban Forsberg, Mattias Thorsell, Erik Janzén and Niklas Rorsman, “Performance Enhancement of Microwave Ga_N HEMTs Without an Al_N-Exclusion Layer Using an Optimized AlGa_N/Ga_N Interface Growth Process” IEEE Transactions on electron devices, **63** (1), January 2016
- [16] Chih-Hao Wang, Shin-Yi Ho and Jian Jang Huang, “Suppression of Current Collapse in Enhancement-Mode AlGa_N/Ga_N High Electron Mobility Transistors” IEEE Electron device letters, **37** (1), January 2016. doi: 10.1109/LED.2015.2498623
- [17] Tian-Li Wu, Denis Marcon, Shuzhen You, Niels Posthuma, Benoit Bakeroort, Steve Stoffels, Marleen Van Hove, Guido Groeseneken and Stefaan Decoutere “Forward Bias Gate Breakdown Mechanism in Enhancement-Mode p-Ga_N Gate AlGa_N/Ga_N High-Electron Mobility Transistors” IEEE Electron device letters, **36** (10), October 2015. Digital Object Identifier 10.1109/LED.2015.2465137
- [18] Xinhua Wang, Sen Huang, Yingkui Zheng, Ke Wei, Xiaojuan Chen, Haoxiang Zhang and Xinyu Liu “Effect of Ga_N Channel Layer Thickness on DC and RF Performance of Ga_N HEMTs With Composite AlGa_N/Ga_N Buffer” IEEE Transactions on electron devices, **61** (5), May 2014. doi: 10.1109/TED.2014.2312232

